

RESEARCH ARTICLE

Inverse optimal control for strict-feedforward nonlinear systems with input delays

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Summary

We consider inverse optimal control for strict-feedforward systems with input delays. A basic predictor control is designed for compensation for this class of nonlinear systems. Furthermore, the proposed predictor control is inverse optimal with respect to a meaningful differential game problem. For a class of linearizable strict-feedforward system, an explicit formula for compensation for input delay, which is also inverse optimal with respect to a meaningful differential game problem, is also acquired. A cart with an inverted pendulum system is given to illustrate the validity of the proposed method.

KEYWORDS

actuator delay, explicit formula, inverse optimality, predictor feedback, strict-feedforward systems

1 | INTRODUCTION

The major progress on feedforward systems was in the work of Mazenc and Praly,¹ which introduced a Lyapunov approach for stabilization of feedforward systems. Further developments on feedforward systems have been acquired by other works.²⁻⁵ For strict-feedforward systems with actuator delay, not only global stability was obtained but also an explicit formula for the predictor state was presented in the work of Krstic.⁶

Predictor-based controls for linear systems with input delays were developed in other works.⁷⁻¹¹ For nonlinear systems with time-varying input delays,¹²⁻¹⁵ as well as wave actuator dynamics with moving boundaries,¹⁶⁻¹⁸ predictor controls have also been achieved. The implementation and approximation issues of predictor-feedback law can be found in the work of Karafyllis and Krstic.¹⁹

The inverse optimality concept is of significant practical importance because it allows the design of optimal control laws without the need to solve a Hamilton-Jacobi-Isaacs partial differential equation that may not be possible to solve.²⁰

In this paper, we extend the results in the work of Krstic⁶ to inverse the optimal control design for strict-feedforward systems. A basic predictor control is designed for compensation for input delay of this class of nonlinear systems first. Furthermore, it is shown that it is inverse optimal with respect to a meaningful differential game problem. An explicit formula for compensation for input delay of a class of linearizable strict-feedforward system, which is also inverse optimal with respect to a meaningful differential game problem, is also acquired.

Notation. We use the common definitions of class \mathcal{K} , \mathcal{K}_∞ , \mathcal{KL} functions from the aforementioned work.⁶ For a vector $X \in R^n$, $\|X\|$ denotes its usual Euclidean norm. For a scalar function $u(\cdot, t) \in L_2(0, 1)$, $\|u(t)\|$ denotes the norm given by $\left(\int_0^1 u^2(x, t) dx\right)^{1/2}$.

2 | GENERAL STRICT-FEEDFORWARD NONLINEAR SYSTEMS

Consider a strict-feedforward nonlinear system with actuator delay

$$\dot{Z}_1(t) = Z_2(t) + \varphi_1(Z_2(t), Z_3(t), \dots, Z_n(t)) + \phi_1(Z_2(t), Z_3(t), \dots, Z_n(t))U(t - D) \quad (1)$$

$$\vdots \quad (2)$$

$$\dot{Z}_{n-2}(t) = Z_{n-1}(t) + \varphi_{n-2}(Z_{n-1}(t), Z_n(t)) + \phi_{n-2}(Z_{n-1}(t), Z_n(t))U(t - D) \quad (3)$$

$$\dot{Z}_{n-1}(t) = Z_n(t) + \phi_{n-1}(Z_n(t))U(t - D) \quad (4)$$

$$\dot{Z}_n(t) = U(t - D), \quad (5)$$

for short,

$$\dot{Z}_i(t) = Z_{i+1}(t) + \varphi_i(\underline{Z}_{i+1}(t)) + \phi_i(\underline{Z}_{i+1}(t))U(t - D), \quad (6)$$

where $i = 1, 2, \dots, n$, $\underline{Z}_j = [Z_j, Z_{j+1}, \dots, Z_n]^T$, $Z_{n+1}(t) = U(t - D)$, $\phi_n = 1$, $\phi_i(0) = 0$, $(\partial\varphi_i(0)/\partial Z_j) = 0$, $\varphi_i(Z_{i+1}, 0, \dots, 0) = 0$, for $i = 1, 2, \dots, n - 1$, $j = i + 1, \dots, n$, and $\underline{Z}_1 \in R^n$ is the state vector, U is a scalar control input, and $D \in R^+$ is an actuator delay.

2.1 | Predictor control for general strict-feedforward nonlinear systems

The nominal control design ($D = 0$) for system (6) is given by Krstic⁶ as

$$U(t) = \alpha_1(Z(t)), \quad (7)$$

where

$$\vartheta_{n+1} = 0, \quad \alpha_{n+1} = 0, \quad (8)$$

and

$$h_i(\underline{Z}_i) = Z_i - \vartheta_{i+1}(\underline{Z}_{i+1}), \quad (9)$$

$$\varpi_i(\underline{Z}_{i+1}) = \phi_i - \sum_{j=i+1}^{n-1} \frac{\partial \vartheta_{i+1}}{\partial Z_j} \phi_j - \frac{\partial \vartheta_{i+1}}{\partial Z_n}, \quad (10)$$

$$\alpha_i(\underline{Z}_i) = \alpha_{i+1} - \varpi_i h_i, \quad (11)$$

$$\vartheta_i(\underline{Z}_i) = - \int_0^\infty \left[\zeta_i^{[i]}(\tau, \underline{Z}_i) + \varphi_{i-1}(\underline{\zeta}_{i-1}^{[i]}(\tau, \underline{Z}_i)) + \phi_{i-1}(\underline{\zeta}_{i-1}^{[i]}(\tau, \underline{Z}_i)) \alpha_i(\underline{\zeta}_i^{[i]}(\tau, \underline{Z}_i)) \right] d\tau, \quad (12)$$

for $i = n, n - 1, \dots, 2, 1$, and the notation in the integrand of (12) refers to the solutions of the subsystem(s)

$$\frac{d}{d\tau} \zeta_j^{[i]} = \zeta_{j+1}^{[i]} + \varphi_j(\underline{\zeta}_{j+1}^{[i]}) + \phi_j(\underline{\zeta}_{j+1}^{[i]}) \alpha_i(\underline{\zeta}_i^{[i]}), \quad (13)$$

for $j = i, i + 1, \dots, n$ at time τ , starting from the initial condition \underline{X}_i . Note that the last of the ϑ 's that need to be computed is ϑ_2 (ϑ_1 is not defined).

Using a transport partial differential equation for representing the actuator state, we represent system (6) as

$$\dot{Z}_i(t) = Z_{i+1}(t) + \varphi_i(\underline{Z}_{i+1}(t)) + \varphi_i(\underline{Z}_{i+1}(t)) u(0, t), \quad (14)$$

$$u_t(x, t) = u_x(x, t), \quad (15)$$

$$u(D, t) = U(t), \quad (16)$$

where $i = 1, 2, \dots, n$, and $u(x, t) = U(t + x - D)$.

The backstepping transformation is given as

$$w(x, t) = u(x, t) - \alpha_1(p(x, t)), \quad (17)$$

where $p(x, t) = [p_1(x, t), p_2(x, t), \dots, p_n(x, t)]^T, x \in [0, D]$ is defined by

$$\frac{\partial p_1(x, t)}{\partial x} = p_2(x, t) + \varphi_1(p_2(x, t), p_3(x, t), \dots, p_n(x, t)) + \phi_1(p_2(x, t), p_3(x, t), \dots, p_n(x, t)) u(x, t) \quad (18)$$

$$\vdots \quad (19)$$

$$\frac{\partial p_{n-2}(x, t)}{\partial x} = p_{n-1}(x, t) + \varphi_{n-2}(p_{n-1}(x, t), p_n(x, t)) + \phi_{n-2}(p_{n-1}(x, t), p_n(x, t)) u(x, t) \quad (20)$$

$$\frac{\partial p_{n-1}(x, t)}{\partial x} = p_n(x, t) + \phi_{n-1}(p_n(x, t)) u(x, t) \quad (21)$$

$$\frac{\partial p_n(x, t)}{\partial x} = u(x, t) \quad (22)$$

with an initial condition

$$p_i(0, t) = Z_i(t), i = 1, 2, \dots, n. \quad (23)$$

From (18)-(23), we have

$$p_n(x, t) = Z_n(t) + \int_0^x u(y, t) dy, \quad (24)$$

$$p_{n-1}(x, t) = Z_{n-1}(t) + \int_0^x (p_n(y, t) + \phi_{n-1}(p_n(y, t)) u(y, t)) dy, \quad (25)$$

for $i = n - 2, n - 3, \dots, 2, 1$, and the predictor solution is obtained recursively as

$$p_i(x, t) = Z_i(t) + \int_0^x (p_{i+1}(y, t) + \varphi_i(p_{i+1}(y, t), \dots, p_n(y, t)) + \phi_i(p_{i+1}(y, t), \dots, p_n(y, t)) u(y, t)) dy. \quad (26)$$

A basic predictor feedback control law for system (14)-(16) is given as

$$U(t) = \frac{c}{c+1} \alpha_1(P(t)) = U^*(t), \quad (27)$$

where $c > 0$ is sufficiently large, and $P(t) = [p_1(D, t), p_2(D, t), \dots, p_n(D, t)]^T$ is acquired by (24)-(26) for $x = D$.

Under the backstepping transformation (17), system (14)-(16) is transferred to a target system as

$$\dot{Z}_i(t) = Z_{i+1}(t) + \varphi_i(\underline{Z}_{i+1}(t)) + \phi_i(\underline{Z}_{i+1}(t)) (w(0, t) + \alpha_1(Z(t))) \quad (28)$$

$$w_t(x, t) = w_x(x, t) \quad (29)$$

$$w(D, t) = U(t) - \alpha_1(p(D, t)). \quad (30)$$

Noting that $p(D, t) = [p_1(D, t), p_2(D, t), \dots, p_n(D, t)]^T$ with the control law (27), (30) can be rewritten as

$$w(D, t) = -\frac{1}{c+1} \alpha_1(P(t)). \quad (31)$$

The inverse transformation of (17) is given for all $x \in [0, D]$ by

$$u(x, t) = w(x, t) + \alpha_1(q(x, t)), \quad (32)$$

where $q(x, t) = [q_1(x, t), q_2(x, t), \dots, q_n(x, t)]^T, x \in [0, D]$ is defined by

$$\frac{\partial q_1(x, t)}{\partial x} = q_2(x, t) + \varphi_1(q_2(x, t), q_3(x, t), \dots, q_n(x, t)) + \phi_1(q_2(x, t), q_3(x, t), \dots, q_n(x, t)) (w(x, t) + \alpha_1(q(x, t))) \quad (33)$$

$$\vdots \quad (34)$$

$$\frac{\partial q_{n-2}(x, t)}{\partial x} = q_{n-1}(x, t) + \varphi_{n-2}(q_{n-1}(x, t), q_n(x, t)) + \phi_{n-2}(q_{n-1}(x, t), q_n(x, t)) (w(x, t) + \alpha_1(q(x, t))) \quad (35)$$

$$\frac{\partial q_{n-1}(x, t)}{\partial x} = q_n(x, t) + \phi_{n-1}(q_n(x, t))(w(x, t) + \alpha_1(q(x, t))) \quad (36)$$

$$\frac{\partial q_n(x, t)}{\partial x} = w(x, t) + \alpha_1(q(x, t)) \quad (37)$$

with an initial condition

$$q_i(0, t) = Z_i(t), i = 1, 2, \dots, n. \quad (38)$$

Under the inverse transformation (32), the target system (28), (29), (31) is transferred to system (14)-(16).

2.2 | Stability analysis of the closed-loop system

Denote the diffeomorphic transformation defined by (9)-(13) as

$$\xi(t) = H(Z(t)). \quad (39)$$

Lemma 1. *There exists a class \mathcal{K} function σ^* such that*

$$\|p(t)\|_{L_\infty[0, D]} \leq \sigma^*(|Z(t)| + \|u(t)\|) \quad (40)$$

for all $t \geq 0$.

Proof. Using similar arguments to the proof in the work of Krstic,⁶ it can be deduced. \square

Lemma 2. *There exists a class \mathcal{K}_∞ function $\underline{\sigma}$ such that*

$$|Z(t)| + \|u(t)\| \leq \underline{\sigma}(|Z(t)| + \|w(t)\|) \quad (41)$$

for all $t \geq 0$.

Proof. Using similar arguments to the proof in the work of Krstic,⁶ it can be deduced. \square

Lemma 3. *There exists a class \mathcal{K} function $\bar{\sigma}$ such that*

$$|Z(t)| + \|w(t)\| \leq \bar{\sigma}(|Z(t)| + \|u(t)\|) \quad (42)$$

for all $t \geq 0$.

Proof. Using similar arguments to the proof in the work of Krstic,⁶ it can be deduced. \square

Note that α_1 is continuous with $\alpha_1(0) = 0$, and there exists a class \mathcal{K}_∞ function ρ_1 such that

$$\alpha_1^2(p(D, t)) \leq \rho_1(|p(D, t)|). \quad (43)$$

Using Lemmas 1 and 2, we have

$$\begin{aligned} \alpha_1^2(p(D, t)) &\leq \rho_1(|p(D, t)|) \\ &\leq \rho_1(\sigma^*(|Z(t)| + \|u(t)\|)) \\ &\leq \rho_1(\sigma^*(\underline{\sigma}(|Z(t)| + \|w(t)\|))) \end{aligned} \quad (44)$$

for all $t \geq 0$.

Denote $\varphi = \rho_1 \circ \sigma^* \circ \underline{\sigma}$, it is easy to know that

$$\alpha_1^2(p(D, t)) \leq \varphi(2|Z(t)|) + \varphi(2\|w(t)\|) \quad (45)$$

for all $t \geq 0$.

Now, we turn our attention to the target system and prove the following result on stability in the sense of its norm.

Lemma 4. *Consider the target system (28), (29), (31). If there exists an $M > 0$ such that*

$$\varphi(2|Z(t)|) \leq M\alpha_1^2(Z(t)), \quad (46)$$

$$\varphi(2\|w(t)\|) \leq M\|w(t)\|^2, \quad (47)$$

for all $t \geq 0$, then there exists $c_1^* > 0$, for all $c > c_1^*$, the target system (28), (29), (31) is asymptotically stable, that is, there exists a \mathcal{KL} function β_1 such that

$$|Z(t)| + \|w(t)\| \leq \beta_1(|Z(0)| + \|w(0)\|, t) \quad (48)$$

for all $t \geq 0$.

Proof. Consider (28) along with the diffeomorphic transformation $\xi(t) = H(Z(t))$ defined by (39). With the observation that $Z_{i+1} + \varphi_i + \phi_i \alpha_{i+1} = \sum_{j=i+1}^n \frac{\partial \theta_{i+1}}{\partial Z_j} (Z_{j+1} + \varphi_j + \phi_j \alpha_{j+1})$, it is easy to verify that $\dot{\xi}_i = \varpi_i (\alpha_1 + w(0, t) + \sum_{j=i+1}^n \varpi_j \xi_j)$, noting from (11) that $\alpha_1 = -\sum_{j=1}^n \varpi_j \xi_j$, we get $\dot{\xi}_i = -\varpi_i^2 \xi_i - \sum_{j=1}^{i-1} \varpi_i \varpi_j \xi_j + \varpi_i w(0, t)$, and it implies that $\dot{\xi}_1 = -\varpi_1^2 \xi_1 + \varpi_1 w(0, t)$. Taking a Lyapunov function $S(t) = \frac{1}{2} \sum_{i=1}^n \xi_i^2(t) = \frac{1}{2} |H(Z)|^2$, we have that

$$\begin{aligned} \dot{S}(t) &= -\frac{1}{2} \sum_{i=1}^n \varpi_i^2 \xi_i^2 - \frac{1}{2} \left(\sum_{i=1}^n \xi_i \varpi_i \right)^2 + w(0, t) \sum_{i=1}^n \varpi_i \xi_i \\ &\leq -\frac{1}{4} \sum_{i=1}^n \varpi_i^2 \xi_i^2 - \frac{1}{2} \left(\sum_{i=1}^n \xi_i \varpi_i \right)^2 + n w^2(0, t). \end{aligned} \tag{49}$$

Consider system (28), (29), (31), an overall Lyapunov function is given as follows:

$$V(t) = S(t) + n \int_0^D e^x w^2(x, t) dx. \tag{50}$$

With (49), we have that

$$\begin{aligned} \dot{V}(t) &= \dot{S}(t) + 2n \int_0^D e^x w(x, t) w_t(x, t) dx \\ &= \dot{S}(t) + n \int_0^D e^x dw^2(x, t) \\ &= \dot{S}(t) + ne^D w^2(D, t) - n w^2(0, t) - n \int_0^D e^x w^2(x, t) dx \\ &\leq -\frac{1}{4} \sum_{i=1}^n \varpi_i^2 \xi_i^2 - \frac{1}{2} \left(\sum_{i=1}^n \xi_i \varpi_i \right)^2 + n w^2(0, t) + ne^D w^2(D, t) - n w^2(0, t) - n \int_0^D e^x w^2(x, t) dx \\ &= -\frac{1}{4} \sum_{i=1}^n \varpi_i^2 \xi_i^2 - \frac{1}{2} \left(\sum_{i=1}^n \xi_i \varpi_i \right)^2 + ne^D w^2(D, t) - n \int_0^D e^x w^2(x, t) dx. \end{aligned} \tag{51}$$

With (31), we have

$$w^2(D, t) = \frac{1}{(c+1)^2} \alpha_1^2(P(t)). \tag{52}$$

Noting that $\alpha_1(Z(t)) = -\sum_{i=1}^n \varpi_i \xi_i$, we get

$$\dot{V}(t) \leq -\frac{1}{4n} \alpha_1^2(Z(t)) - \frac{1}{2} \alpha_1^2(Z(t)) + \frac{ne^D \alpha_1^2(P(t))}{(c+1)^2} - n \|w(t)\|^2. \tag{53}$$

With the help of (46), (47), it holds

$$\begin{aligned} \dot{V}(t) &\leq -\left(\frac{1}{4n} + \frac{1}{2}\right) \alpha_1^2(Z(t)) + \frac{ne^D (\varphi(2|Z(t)|) + \varphi(2\|w(t)\|))}{(c+1)^2} - n \|w(t)\|^2 \\ &\leq -\left(\left(\frac{1}{4n} + \frac{1}{2}\right) - \frac{ne^D M}{(c+1)^2}\right) \alpha_1^2(Z(t)) - \left(n - \frac{ne^D M}{(c+1)^2}\right) \|w(t)\|^2. \end{aligned} \tag{54}$$

Choosing

$$c_1^* = 2n \sqrt{2M} e^{D/2} \tag{55}$$

for all $c > c_1^*$, one has

$$\dot{V}(t) \leq -\left(\frac{1}{8n} + \frac{1}{4}\right) \alpha_1^2(Z(t)) - \frac{n}{2} \|w(t)\|^2, \tag{56}$$

so the target system (28), (29), (31) is asymptotically stable. Since the function $\alpha_1^2(Z(t))$ is positive definite in $Z(t)$, there exists a class \mathcal{K} function γ_1 such that $\dot{V}(t) \leq -\gamma_1(V(t))$. Then, there exists a class \mathcal{KL} function β_2 such that $V(t) \leq \beta_2(V(0), t)$ for all $t \geq 0$. With additional routine class \mathcal{K} calculations, one finds β_1 that completes the proof of the lemma. \square

Theorem 1. Consider the closed-loop system consisting of (14)-(16) together with the control law (27). If there exists a $M > 0$ such that (46), (47) hold, then there exists $c_1^* > 0$ given by (55), for all $c > c_1^*$, the closed-loop system of (14)-(16), (27) is asymptotically stable, that is, there exists a class \mathcal{KL} function β_3 such that

$$|Z(t)| + \|u(t)\| \leq \beta_3(|Z(0)| + \|u(0)\|, t) \quad (57)$$

for all $t \geq 0$.

Proof. Using Lemmas 2, 3, and 4, we have

$$\begin{aligned} & |Z(t)| + \|u(t)\| \\ & \leq \underline{\sigma}(|Z(t)| + \|w(t)\|) \\ & \leq \underline{\sigma}(\beta_1(|Z(0)| + \|w(0)\|), t) \\ & \leq \underline{\sigma}(\beta_1(\bar{\sigma}(|Z(0)| + \|u(0)\|), t)) \end{aligned} \quad (58)$$

for all $t \geq 0$. Denote that $\beta_3(s, t) = \underline{\sigma}(\beta_1(\bar{\sigma}(s), t))$, (57) is drawn. Hence, the closed-loop system of (14)-(16), (27) is asymptotically stable.

Theorem 2. Consider the closed-loop system consisting of (1)-(5) together with the control law (27). If there exists an $M > 0$ such that (46), (47) hold, then there exists $c_1^* > 0$ given by (55), for all $c > c_1^*$, the closed-loop system of (1)-(5), (27) is asymptotically stable, that is, there exists a class \mathcal{KL} function β_4 such that

$$|Z(t)| + \left(\int_{t-D}^t U^2(\theta) d\theta \right)^{1/2} \leq \beta_4 \left(\|Z(0)\| + \left(\int_{-D}^0 U^2(\theta) d\theta \right)^{1/2}, t \right) \quad (59)$$

for all $t \geq 0$. □

Proof. Using Theorem 1, we get

$$\begin{aligned} & |Z(t)| + \left(\int_{t-D}^t U^2(\theta) d\theta \right)^{1/2} \\ & = |Z(t)| + \|u(t)\| \\ & \leq \beta_3(|Z(0)| + \|u(0)\|, t) \\ & = \beta_3 \left(|Z(0)| + \left(\int_{-D}^0 U^2(\theta) d\theta \right)^{1/2}, t \right) \end{aligned} \quad (60)$$

for all $t \geq 0$. Choosing $\beta_4 = \beta_3$, (59) is obtained. Hence, the closed-loop system of (1)-(5), (27) is asymptotically stable. □

2.3 | Inverse optimal control for general strict-feedforward nonlinear systems

Theorem 3. Consider the closed-loop system consisting of (14)-(16) together with the control law (27). If there exists an $M > 0$ such that (46), (47) hold, then there exists $c_1^{**} > c_1^* > 0$, for all $c > c_1^{**}$, the control law (27) minimizes the cost functional

$$J = \lim_{t \rightarrow \infty} \left(\gamma V(t) + \int_0^t \left(L(\tau) + \frac{\gamma n e^D}{c} U^2(\tau) \right) d\tau \right), \quad (61)$$

where $V(t)$ is given by (50), and L is a functional of $(Z(t), U(\theta))$ for all $t - D \leq \theta \leq t$ such that

$$L(t) \geq \gamma \left(\frac{\alpha_1^2(Z(t))}{8n} + \frac{n}{2} \|w(t)\|^2 \right) \quad (62)$$

for an arbitrary $\gamma > 0$.

Proof. Let

$$L(t) = -\frac{\gamma n e^D}{c+1} \alpha_1^2(P(t)) + \gamma \left(\frac{1}{2} \sum_{i=1}^n \varpi_i^2 \xi_i^2 + \frac{1}{2} \left(\sum_{i=1}^n \xi_i \varpi_i \right)^2 - w(0, t) \sum_{i=1}^n \varpi_i \xi_i + n w^2(0, t) + n \int_0^D e^x w^2(x, t) dx \right). \quad (63)$$

It can be deduced that

$$L(t) \geq -\frac{\gamma ne^D}{c+1} \alpha_1^2(P(t)) + \frac{\gamma}{4} \sum_{i=1}^n \varpi_i^2 \xi_i^2 + \frac{\gamma}{2} \left(\sum_{i=1}^n \xi_i \varpi_i \right)^2 + n\gamma \int_0^D e^x w^2(x, t) dx. \tag{64}$$

With the help of (46), (47), there exists

$$c_1^{**} = 8n^2 M e^D \tag{65}$$

for all $c > c_1^{**}$, one has

$$L(t) \geq \frac{\gamma}{8n} \alpha_1^2(Z(t)) + \frac{n\gamma}{2} \|w(t)\|^2 \tag{66}$$

for any $t \geq 0$.

With the help of (49), (51), after some calculations, and noting $U^*(t) = \frac{c}{c+1} \alpha_1(P(t))$, we have

$$\begin{aligned} L(t) &= -\frac{\gamma ne^D}{c+1} \alpha_1^2(P(t)) + \gamma \left(\frac{1}{2} \sum_{i=1}^n \varpi_i^2 \xi_i^2 + \frac{1}{2} \left(\sum_{i=1}^n \xi_i \varpi_i \right)^2 - w(0, t) \sum_{i=1}^n \varpi_i \xi_i + n w^2(0, t) + n \int_0^D e^{gx} w^2(x, t) dx \right) \\ &= -\frac{\gamma ne^D}{c+1} \alpha_1^2(P(t)) + \gamma ne^D w^2(D, t) - \gamma \dot{V}(t) \\ &= -\frac{\gamma ne^D}{c+1} \alpha_1^2(P(t)) + \gamma ne^D (U(t) - \alpha_1(P(t)))^2 - \gamma \dot{V}(t) \\ &= -\frac{\gamma ne^D (c+1)}{c^2} (U^*(t))^2 + \gamma ne^D \left(U(t) - \frac{c+1}{c} U^*(t) \right)^2 - \gamma \dot{V}(t) \\ &= \frac{\gamma ne^D}{c} (U^*(t))^2 + \gamma ne^D \left((U(t) - U^*(t))^2 - \frac{2}{c} U(t) U^*(t) \right) - \gamma \dot{V}(t), \end{aligned} \tag{67}$$

and hence, it can be deduced that

$$\gamma V(t) + \int_0^t \left(L(\tau) + \frac{\gamma ne^D}{c} U^2(\tau) \right) d\tau = \gamma V(0) + \gamma \int_0^t ne^D \left(1 + \frac{1}{c} \right) (U(t) - U^*(t))^2 d\tau \tag{68}$$

so the minimum of (61) is reached with

$$U(t) = U^*(t) \tag{69}$$

such that

$$J = \gamma V(0). \tag{70}$$

□

Remark 1. c_1^{**} given by (65) is bigger than c_1^* defined by (55).

3 | LINEARIZABLE STRICT-FEEDFORWARD SYSTEMS

From the work of Krstic,⁶ it was shown that a strict-feedforward system (1)-(5) for $D = 0$ is linearizable provided the following assumption is satisfied.

Assumption 1. The functions $\varphi_i(\underline{Z}_{i+1})$ and $\phi_i(\underline{Z}_{i+1})$ can be written as $\phi_{n-1}(Z_n) = \theta'_n(Z_n)$ and $\varphi_{n-1}(Z_n) = 0$, and

$$\phi_i(\underline{Z}_{i+1}) = \sum_{j=i+1}^{n-1} \frac{\partial \theta_{i+1}(\underline{Z}_{i+1})}{\partial Z_j} \phi_j(\underline{Z}_{j+1}) + \frac{\partial \theta_{i+1}(\underline{Z}_{i+1})}{\partial Z_n} \tag{71}$$

$$\varphi_i(\underline{Z}_{i+1}) = \sum_{j=i+1}^{n-1} \frac{\partial \theta_{i+1}(\underline{Z}_{i+1})}{\partial Z_j} \left(Z_{j+1} + \varphi_j(\underline{Z}_{j+1}) \right) - \theta_{i+2}(\underline{Z}_{i+2}) \tag{72}$$

for $i = n-2, \dots, 1$, using some C^1 scalar-valued functions $\theta_i(\underline{Z}_i)$ satisfying $\theta_i(0) = (\partial \theta_i(0) / \partial Z_j) = 0$, for $i = 2, \dots, n, j = i, \dots, n$.

The nominal control design ($D = 0$) for linearizable strict-feedforward (1)-(5) is given by Krstic⁶ as

$$U(t) = \alpha_1(Z(t)), \tag{73}$$

where $\vartheta_{n+1} = 0$, $\alpha_{n+1} = 0$, and, for $i = n, n-1, \dots, 2, 1$,

$$\alpha_i(\underline{Z}_i) = -\sum_{j=i}^n \left(Z_j - \vartheta_{j+1}(\underline{Z}_{j+1}) \right), \quad (74)$$

$$\zeta_n^{[i]}(\tau, \underline{Z}_i) = e^{-\tau} \sum_{k=0}^{n-i} \frac{(-\tau)^k}{k!} (Z_{n-k} - \vartheta_{n-k+1}(\underline{Z}_{n-k+1})) \quad (75)$$

$$\zeta_j^{[i]}(\tau, \underline{Z}_i) = e^{-\tau} \sum_{k=0}^{j-i} \frac{(-\tau)^k}{k!} (Z_{j-k} - \vartheta_{j-k+1}(\underline{Z}_{j-k+1})) + \vartheta_{j+1}(\zeta_{j+1}^{[i]}(\tau, \underline{Z}_i)) \quad (76)$$

$$\vartheta_i(\underline{Z}_i) = -\int_0^\infty \left[\zeta_i^{[i]}(\tau, \underline{Z}_i) + \varphi_{i-1}(\zeta_{i-1}^{[i]}(\tau, \underline{Z}_i)) + \phi_{i-1}(\zeta_{i-1}^{[i]}(\tau, \underline{Z}_i)) \alpha_i(\zeta_{i-1}^{[i]}(\tau, \underline{Z}_i)) \right] d\tau. \quad (77)$$

3.1 | Predictor control for linearizable strict-feedforward systems

Consider the linearizable strict-feedforward system with actuator delay

$$\dot{Z}_i(t) = Z_{i+1}(t) + \varphi_i(\underline{Z}_{i+1}(t)) + \phi_i(\underline{Z}_{i+1}(t)) u(0, t) \quad (78)$$

$$u_t(x, t) = u_x(x, t) \quad (79)$$

$$u(D, t) = U(t), \quad (80)$$

where $i = 1, 2, \dots, n$.

With the diffeomorphic transformation $h = G(Z)$ defined by

$$h_n = Z_n \quad (81)$$

$$h_i = \sum_{j=i}^n \binom{n-i}{j-i} (-1)^{j-i} (Z_j - \vartheta_{j+1}(\underline{Z}_{j+1})), \quad i = n-1, n-2, \dots, 1 \quad (82)$$

and $\vartheta_j, j = 1, 2, \dots, n$ given by (74)-(77), system (78)-(80) is transferred to the following system:

$$\dot{h}_i(t) = h_{i+1}(t), \quad i = 1, 2, \dots, n-1, \quad (83)$$

$$\dot{h}_n(t) = u(0, t) \quad (84)$$

$$u_t(x, t) = u_x(x, t) \quad (85)$$

$$u(D, t) = U(t). \quad (86)$$

The predictor feedback for system (83)-(86) is

$$U(t) = \frac{c}{c+1} \alpha_1(G^{-1}(\eta(D, t))) = -\frac{c}{c+1} \sum_{i=1}^n \binom{n}{i-1} \eta_i(D, t) = U^*(t), \quad (87)$$

where $c > 0$ is sufficiently large, and $\eta(D, t) = [\eta_1(D, t), \dots, \eta_n(D, t)]^T$ is given by

$$\frac{\partial}{\partial x} \eta_i(x, t) = \eta_{i+1}(x, t), \quad i = 1, 2, \dots, n-1, \quad (88)$$

$$\frac{\partial}{\partial x} \eta_n(x, t) = u(x, t) \quad (89)$$

with initial condition $\eta(0, t) = h(t)$ for $x = D$.

It can be deduced that

$$\eta_i(x, t) = \sum_{j=i}^n \frac{x^{j-i}}{(j-i)!} h_j(t) + \int_0^x \frac{(x-y)^{n+1-i}}{(n+1-i)!} u(y, t) dy, \quad (90)$$

for $i = 1, 2, \dots, n$. By (81)-(82), we have

$$\eta_i(x, t) = \sum_{j=i}^n \frac{x^{j-i}}{(j-i)!} \sum_{l=j}^n \binom{n-j}{l-j} (-1)^{l-j} (Z_l - \vartheta_{l+1}(\underline{Z}_{l+1})) + \int_0^x \frac{(x-y)^{n+1-i}}{(n+1-i)!} u(y, t) dy, \quad (91)$$

for $i = 1, 2, \dots, n$. Hence, the feedback law for system (83)-(86) can be rewritten as

$$U(t) = -\frac{c}{c+1} \sum_{i=1}^n \binom{n}{i-1} \left(\sum_{j=i}^n \frac{D^{j-i}}{(j-i)!} \sum_{l=j}^n \binom{n-j}{l-j} (-1)^{l-j} (Z_l - \vartheta_{l+1}(Z_{l+1})) + \int_0^D \frac{(D-y)^{n+1-i}}{(n+1-i)!} u(y, t) dy \right). \quad (92)$$

Noting that $u(x, t) = U(x + t - D)$, the predictor control law for system (78)-(80) is

$$U(t) = -\frac{c}{c+1} \sum_{i=1}^n \binom{n}{i-1} \left(\sum_{j=i}^n \frac{D^{j-i}}{(j-i)!} \sum_{l=j}^n \binom{n-j}{l-j} (-1)^{l-j} (Z_l - \vartheta_{l+1}(Z_{l+1})) \int_{t-D}^t \frac{(D-y)^{n+1-i}}{(n+1-i)!} U(\sigma) d\sigma \right), \quad (93)$$

where $c > 0$ is sufficiently large.

Next, we will prove that the closed-loop system consisting of (78)-(80) together with the control law (93) is asymptotically stable.

With a diffeomorphic transformation

$$\xi_{n-i} = \sum_{j=0}^i \binom{i}{j} h_{n-j}, \quad i = 0, 1, 2, \dots, n-1, \quad (94)$$

system (83)-(86) is transferred to

$$\dot{\xi}_i(t) = \sum_{j=i+1}^n \xi_j(t) + u(0, t), \quad i = 1, 2, \dots, n-1 \quad (95)$$

$$\dot{\xi}_n(t) = u(0, t) \quad (96)$$

$$u_t(x, t) = u_x(x, t) \quad (97)$$

$$u(D, t) = U(t), \quad (98)$$

and it can be deduced that

$$\sum_{i=1}^n \binom{n}{i-1} h_i(t) = \sum_{i=1}^n \xi_i(t). \quad (99)$$

The infinite-dimensional backstepping transformation is defined as follows:

$$w(x, t) = u(x, t) + \sum_{i=1}^n \binom{n}{i-1} \eta_i(x, t), \quad (100)$$

where $\eta_i(x, t), i = 1, 2, \dots, n$ are given by (90).

Noting that $\eta_i(0, t) = h_i(t)$, with the help of (87), (98)-(100), system (95)-(98) is transferred to the target system

$$\dot{\xi}_i(t) = -\sum_{j=1}^i \xi_j(t) + w(0, t), \quad i = 1, 2, \dots, n \quad (101)$$

$$w_t(x, t) = w_x(x, t) \quad (102)$$

$$w(D, t) = \frac{1}{c} \sum_{i=1}^n \binom{n}{i-1} \eta_i(D, t). \quad (103)$$

The inverse backstepping transformation of (100) is defined as follows:

$$u(x, t) = w(x, t) - \sum_{i=1}^n \varpi_i(x, t), \quad (104)$$

where

$$\frac{\partial}{\partial x} \varpi_i(x, t) = -\sum_{j=1}^i \varpi_j(x, t) + w(x, t), \quad i = 1, 2, \dots, n \quad (105)$$

with initial condition $\varpi_i(0, t) = \xi(t)$.

Under the inverse backstepping transformation (104), the target system (101)-(103) is transferred to system (95)-(98).

Lemma 5. Consider the target system (101)-(103), there exists $c^* > 0$ such that system (101)-(103) is asymptotically stable for all $c > c^*$, that is, there exist $R > 0, \bar{\lambda} > 0$, such that for all $c > c^*$,

$$|\xi(t)|^2 + \|w(t)\|^2 \leq Re^{-\bar{\lambda}t}(|\xi(0)|^2 + \|w(0)\|^2) \tag{106}$$

for all $t \geq 0$.

Proof. Denote

$$A = \begin{bmatrix} -1 & 0 & 0 & \cdots & 0 \\ -1 & -1 & 0 & \cdots & 0 \\ \vdots & \vdots & \ddots & \ddots & \vdots \\ -1 & -1 & \cdots & -1 & 0 \\ -1 & -1 & -1 & \cdots & -1 \end{bmatrix}, B = \begin{bmatrix} 1 \\ \vdots \\ 1 \\ 1 \\ 1 \end{bmatrix}. \tag{107}$$

Since A is a Hurwitz matrix, for any a positive matrix Q , there exists a positive matrix P such that $AP + PA^T = -Q$.

Considering system (101)-(103), an overall Lyapunov function is given as follows:

$$V(t) = \xi^T P \xi + l \int_0^D e^x w^2(x, t) dx, \tag{108}$$

where $l > \frac{2\lambda_{\max}(PBB^T P)}{\lambda_{\min}(Q)}$. We have that

$$\begin{aligned} \dot{V}(t) &= \xi^T (AP + PA^T) \xi + 2\xi^T PBw(0, t) + 2l \int_0^D e^x w(x, t) w_t(x, t) dx \\ &= -\xi^T Q \xi + 2\xi^T PBw(0, t) + 2l \int_0^D e^x w(x, t) w_t(x, t) dx \\ &\leq -\lambda_{\min}(Q) \xi^T \xi + \frac{\lambda_{\min}(Q)}{2\lambda_{\max}(PBB^T P)} \xi^T PBB^T P \xi + \frac{2\lambda_{\max}(PBB^T P)}{\lambda_{\min}(Q)} w^2(0, t) + l \int_0^D e^x dw^2(x, t) \\ &\leq -\frac{\lambda_{\min}(Q)}{2} \xi^T \xi + \frac{2\lambda_{\max}(PBB^T P)}{\lambda_{\min}(Q)} w^2(0, t) + le^D w^2(D, t) - lw^2(0, t) - l \int_0^D e^x w^2(x, t) dx \\ &\leq -\frac{\lambda_{\min}(Q)}{2} \xi^T \xi + le^D w^2(D, t) - l \int_0^D e^x w^2(x, t) dx \\ &\leq -\frac{\lambda_{\min}(Q)}{2} |\xi|^2 + le^D w^2(D, t) - l \|w(t)\|^2. \end{aligned} \tag{109}$$

From (103), we have

$$w^2(D, t) = \frac{1}{c^2} \left(\sum_{i=1}^n \binom{n}{i-1} \eta_i(D, t) \right)^2. \tag{110}$$

Using (90), we get

$$\begin{aligned} \eta_i(D, t) &\leq \left| \sum_{j=i}^n \frac{D^{j-i}}{(j-i)!} h_j(t) \right| + \left| \int_0^D \frac{(D-y)^{n+1-i}}{(n+1-i)!} u(y, t) dy \right| \\ &\leq e^D |h(t)| + \frac{D^{n+1-i}}{(n+1-i)!} \sqrt{D} \|u(t)\| \\ &\leq e^D |h(t)| + \max \left\{ D, \frac{D^2}{2!}, \dots, \frac{D^n}{n!} \right\} \sqrt{D} \|u(t)\|, \end{aligned} \tag{111}$$

so

$$w^2(D, t) \leq \frac{1}{c^2} (2^n - 1)^2 (2e^{2D} |h(t)|^2 + 2\varsigma D \|u(t)\|^2), \tag{112}$$

where

$$\varsigma = \left(\max \left\{ D, \frac{D^2}{2!}, \dots, \frac{D^n}{n!} \right\} \right)^2. \tag{113}$$

It can be deduced that the inverse of (94) is

$$h_{n-i}(t) = \sum_{j=0}^i (-1)^{i+j} \binom{i}{j} \xi_{n-j}(t), \quad i = 0, 1, 2, \dots, n-1, \tag{114}$$

and after some calculation, we have

$$|h(t)| \leq \frac{\sqrt{4^n - 1}}{\sqrt{3}} |\xi(t)|. \tag{115}$$

It is easy to get from (105) that

$$\varpi(x, t) = e^{Ax} \xi(t) + \int_0^x e^{A(x-s)} Bw(s, t) ds, \tag{116}$$

where A and B are given by (107). Furthermore, we get

$$\begin{aligned} |\varpi(x, t)|^2 &\leq 2e^{2|A|x} |\xi(t)|^2 + 2 \left| \int_0^x e^{A(x-s)} Bw(s, t) ds \right|^2 \\ &\leq 2e^{2|A|x} |\xi(t)|^2 + 2 \int_0^x |e^{A(x-s)} B|^2 ds \int_0^x w^2(s, t) ds \\ &\leq 2e^{2|A|x} |\xi(t)|^2 + 2|B|^2 \int_0^x e^{2|A|(x-s)} ds \int_0^x w^2(s, t) ds \\ &= 2e^{2|A|x} |\xi(t)|^2 + |B|^2 \frac{e^{2|A|x} - 1}{|A|} \int_0^x w^2(s, t) ds. \end{aligned} \tag{117}$$

Using (104), we have

$$\begin{aligned} u^2(x, t) &\leq 2w^2(x, t) + 2 \left(\sum_{i=1}^n \varpi_i(x, t) \right)^2 \\ &\leq 2w^2(x, t) + 2n \sum_{i=1}^n \varpi_i^2(x, t) \\ &= 2w^2(x, t) + 2n |\varpi(x, t)|^2. \end{aligned} \tag{118}$$

By (117), (118), it can be deduced that

$$\|u(t)\|^2 \leq 2\|w(t)\|^2 + \frac{2n(e^{2|A|D} - 1)}{|A|} |\xi(t)|^2 + \frac{2n|B|^2}{|A|} \left(\frac{e^{2|A|D} - 1}{2|A|} - D \right) \|w(t)\|^2. \tag{119}$$

With the help of (112), (115), (119), we arrive at

$$\begin{aligned} w^2(D, t) &\leq \frac{1}{c^2} (2^n - 1)^2 \left(\frac{2e^{2D}(4^n - 1)}{3} |\xi(t)|^2 + 2\zeta D \|u(t)\|^2 \right) \\ &\leq \frac{2(2^n - 1)^2 e^{2D}(4^n - 1)}{c^2} |\xi(t)|^2 \\ &\quad + \frac{2(2^n - 1)^2}{c^2} \zeta D \left(2\|w(t)\|^2 + \frac{2n(e^{2|A|D} - 1)}{|A|} |\xi(t)|^2 + \frac{2n|B|^2}{|A|} \left(\frac{e^{2|A|D} - 1}{2|A|} - D \right) \|w(t)\|^2 \right) \\ &= \frac{2(2^n - 1)^2}{c^2} \left(\frac{e^{2D}(4^n - 1)}{3} + \frac{2n\zeta D(e^{2|A|D} - 1)}{|A|} \right) |\xi(t)|^2 \\ &\quad + \frac{4(2^n - 1)^2}{c^2} \zeta D \left(1 + \frac{n|B|^2}{|A|} \left(\frac{e^{2|A|D} - 1}{2|A|} - D \right) \right) \|w(t)\|^2, \end{aligned} \tag{120}$$

where ζ is given by (113). Using (109), (120), we get

$$\begin{aligned} \dot{V}(t) &\leq -\frac{\lambda_{\min}(Q)}{2} |\xi(t)|^2 + \frac{2(2^n - 1)^2 l e^D}{c^2} \left(\frac{e^{2D}(4^n - 1)}{3} + \frac{2n\zeta D(e^{2|A|D} - 1)}{|A|} \right) |\xi(t)|^2 \\ &\quad + \frac{4l e^D (2^n - 1)^2}{c^2} \zeta D \left(1 + \frac{n|B|^2}{|A|} \left(\frac{e^{2|A|D} - 1}{2|A|} - D \right) \right) \|w(t)\|^2 - l \|w(t)\|^2. \end{aligned} \tag{121}$$

Choosing

$$c^* = 2\sqrt{2}(2^n - 1)e^{\frac{D}{2}} \max \left\{ \sqrt{\frac{le^{2D}(4^n - 1)}{3\lambda_{\min}(Q)} + \frac{2nl\zeta D (e^{2|A|D} - 1)}{|A|\lambda_{\min}(Q)}}, \sqrt{\zeta D \left(1 + \frac{n|B|^2}{|A|} \left(\frac{e^{2|A|D} - 1}{2|A|} - D \right) \right)} \right\} \quad (122)$$

for all $c > c^*$, we get

$$\begin{aligned} \dot{V}(t) &\leq -\frac{\lambda_{\min}(Q)}{4} |\xi(t)|^2 - \frac{l}{2} \|w(t)\|^2 \\ &\leq -\min \left\{ \frac{\lambda_{\min}(Q)}{4}, \frac{l}{2} \right\} \{ |\xi(t)|^2 + \|w(t)\|^2 \}. \end{aligned} \quad (123)$$

With (108), we have

$$\begin{aligned} &\min \{ \lambda_{\min}(P), l \} (|\xi(t)|^2 + \|w(t)\|^2) \\ &\leq V(t) \\ &\leq \max \{ \lambda_{\max}(P), le^D \} (|\xi(t)|^2 + \|w(t)\|^2). \end{aligned} \quad (124)$$

Thus, from (123), (124), it holds that

$$\dot{V}(t) \leq -\bar{\lambda}V(t) \quad (125)$$

with

$$\bar{\lambda} = \frac{\min \left\{ \frac{\lambda_{\min}(Q)}{4}, \frac{l}{2} \right\}}{\max \{ \lambda_{\max}(P), le^D \}}. \quad (126)$$

We arrive at

$$\begin{aligned} V(t) &\leq e^{-\bar{\lambda}t}V(0) \\ &\leq e^{-\bar{\lambda}t} \max \{ \lambda_{\max}(P), le^D \} (|\xi(0)|^2 + \|w(0)\|^2). \end{aligned} \quad (127)$$

With the help of (124), we have

$$\begin{aligned} |\xi(t)|^2 + \|w(t)\|^2 &\leq \frac{V(t)}{\min \{ \lambda_{\min}(P), l \}} \\ &\leq \frac{\max \{ \lambda_{\max}(P), le^D \}}{\min \{ \lambda_{\min}(P), l \}} e^{-\bar{\lambda}t} (|\xi(0)|^2 + \|w(0)\|^2). \end{aligned} \quad (128)$$

Thus, for all $c > c^*$, we get (106) where $c^*, \bar{\lambda}$ are given by (122) and (126), respectively, and $R = \frac{\max \{ \lambda_{\max}(P), le^D \}}{\min \{ \lambda_{\min}(P), l \}}$. The proof is completed. \square

Lemma 6. *Considering system (83)-(86), there exists $c^* > 0$ such that system (83)-(86) is asymptotically stable for all $c > c^*$, that is, there exist $\bar{R} > 0, \bar{\lambda} > 0$, such that for all $c > c^*$,*

$$\|h(t)\|^2 + \|u(t)\|^2 \leq \bar{R}e^{-\bar{\lambda}t} (\|h(0)\|^2 + \|u(0)\|^2) \quad (129)$$

for all $t \geq 0$.

Proof. With the help of (94), we get

$$|\xi(t)| \leq \frac{\sqrt{4^n - 1}}{\sqrt{3}} |h(t)|. \quad (130)$$

Using (90), we have

$$\begin{aligned} \eta_i(x, t) &\leq \left| \sum_{j=i}^n \frac{x^{j-i}}{(j-i)!} h_j(t) \right| + \left| \int_0^x \frac{(x-y)^{n+1-i}}{(n+1-i)!} u(y, t) dy \right| \\ &\leq e^x |h(t)| + \frac{x^{n+1-i}}{(n+1-i)!} \sqrt{x} \|u(t)\| \\ &\leq e^x |h(t)| + \max \left\{ x, \frac{x^2}{2!}, \dots, \frac{x^n}{n!} \right\} \sqrt{x} \|u(t)\| \\ &\leq e^x |h(t)| + e^x \sqrt{x} \|u(t)\|, \end{aligned} \quad (131)$$

with $i = 1, 2, \dots, n$. By (100), it can be deduced that

$$\begin{aligned} \|w(t)\|^2 &= \int_0^D w^2(x, t) dx \\ &\leq 2 \int_0^D u^2(x, t) dx + 2 \int_0^D \left(\sum_{i=1}^n \binom{n}{i-1} \eta_i(x, t) \right)^2 dx \\ &\leq 2\|u(t)\|^2 + 4(2^n - 1)^2 \int_0^D (e^{2x}|h(t)|^2 + e^{2x}x\|u(t)\|^2) dx \\ &= (2 + 2(2^n - 1)^2 (De^{2D} - e^{2D} + 1)) \|u(t)\|^2 + 2(2^n - 1)^2(e^{2D} - 1)|h(t)|^2. \end{aligned} \tag{132}$$

We deduce from (115), (119) that

$$\begin{aligned} |h(t)|^2 + \|u(t)\|^2 &\leq \left(\frac{4^n - 1}{3} + \frac{2n(e^{2|A|D} - 1)}{|A|} \right) |\xi(t)|^2 \\ &\quad + \left(2 + \frac{2n|B|^2}{|A|} \left(\frac{e^{2|A|D} - 1}{2|A|} - D \right) \right) \|w(t)\|^2 \\ &\leq \Lambda_1 (|\xi(t)|^2 + \|w(t)\|^2), \end{aligned} \tag{133}$$

where

$$\Lambda_1 = \max \left\{ \frac{4^n - 1}{3} + \frac{2n(e^{2|A|D} - 1)}{|A|}, 2 + \frac{2n|B|^2}{|A|} \left(\frac{e^{2|A|D} - 1}{2|A|} - D \right) \right\}. \tag{134}$$

Using Lemma 5, there exist $R > 0, \bar{\lambda} > 0$, such that for all $c > c^*$,

$$\begin{aligned} |h(t)|^2 + \|u(t)\|^2 &\leq \Lambda_1 (|\xi(t)|^2 + \|w(t)\|^2) \\ &\leq \Lambda_1 R e^{-\bar{\lambda}t} (|\xi(0)|^2 + \|w(0)\|^2) \end{aligned} \tag{135}$$

for all $t \geq 0$. With the help of (115), (132), we get

$$\begin{aligned} |h(t)|^2 + \|u(t)\|^2 &\leq \Lambda_1 R e^{-\bar{\lambda}t} (|\xi(0)|^2 + \|w(0)\|^2) \\ &\leq \Lambda_1 R e^{-\bar{\lambda}t} \left(\frac{4^n - 1}{3} + 2(2^n - 1)^2(e^{2D} - 1) \right) |h(0)|^2 \\ &\quad + \Lambda_1 R e^{-\bar{\lambda}t} (2 + 2(2^n - 1)^2(De^{2D} - e^{2D} + 1)) \|u(0)\|^2 \\ &\leq \Lambda_1 \Lambda_2 R e^{-\bar{\lambda}t} (|h(0)|^2 + \|u(0)\|^2) \end{aligned} \tag{136}$$

for all $t \geq 0$, with

$$\Lambda_2 = \max \left\{ \frac{4^n - 1}{3} + 2(2^n - 1)^2 (e^{2D} - 1), 2 + 2(2^n - 1)^2 (De^{2D} - e^{2D} + 1) \right\}. \tag{137}$$

Denote

$$\bar{R} = R\Lambda_1\Lambda_2, \tag{138}$$

(129) is drawn. The proof is completed. \square

Theorem 4. Consider the closed-loop system consisting of (78)-(80) together with the control law (87). Under Assumption 1, there exist $c^* > 0$ and a \mathcal{KL} function β_5 , such that for all $c > c^*$,

$$|Z(t)|^2 + \int_{t-D}^t U^2(\sigma) d\sigma \leq \beta_5 \left(|Z(0)|^2 + \int_{-D}^0 U^2(\sigma) d\sigma, t \right) \tag{139}$$

for all $t \geq 0$.

Proof. With the diffeomorphic transformation $h(t) = G(Z(t))$ defined by (81)-(82), there exist \mathcal{K} functions γ_1, γ_2 such that

$$|Z(t)|^2 = |G^{-1}(h(t))|^2 \leq \gamma_1 (|h(t)|^2), \tag{140}$$

$$|h(t)|^2 = |G(Z(t))|^2 \leq \gamma_2 (|Z(t)|^2). \tag{141}$$

Using Lemma 6, there exists $c^* > 0$ such that the closed-loop system (78)-(80) together with the control law (87) holds that

$$\begin{aligned}
|Z(t)|^2 + \int_{t-D}^t U^2(\sigma) d\sigma &= |Z(t)|^2 + \|u(t)\|^2 \\
&\leq \gamma_1 (|h(t)|^2) + \|u(t)\|^2 \\
&\leq \gamma_3 (|h(t)|^2 + \|u(t)\|^2) \\
&\leq \gamma_3 \left(\bar{R} e^{-\bar{\lambda} t} (|h(0)|^2 + \|u(0)\|^2) \right) \\
&\leq \gamma_3 \left(\bar{R} e^{-\bar{\lambda} t} (\gamma_2 |Z(0)|^2 + \|u(0)\|^2) \right) \\
&\leq \gamma_3 \left(\bar{R} e^{-\bar{\lambda} t} (\gamma_4 (|Z(0)|^2 + \|u(0)\|^2)) \right) \\
&\leq \gamma_3 \left(\bar{R} e^{-\bar{\lambda} t} \left(\gamma_4 \left(|Z(0)|^2 + \int_{-D}^0 U^2(\sigma) d\sigma \right) \right) \right)
\end{aligned} \tag{142}$$

for all $t \geq 0$, with $\gamma_3(s) = \gamma_1(s) + s, \gamma_4(s) = \gamma_2(s) + s$. Choosing $\beta_5(s, t) = \gamma_3(\bar{R} e^{-\bar{\lambda} t} (\gamma_4(s)))$, where $\bar{\lambda}, \bar{R}$ are given by (126), (138), respectively, (139) is obtained. The proof is completed. \square

3.2 | Inverse optimal control for linearizable strict-feedforward systems

Theorem 5. Consider the closed-loop system consisting of (78)-(80) together with the control law (87). Under Assumption 1, there exists a sufficiently large $c^{**} > c^* > 0$, for all $c > c^{**}$, the control law (87) minimizes the cost functional

$$J = \lim_{t \rightarrow \infty} \left(\gamma V(t) + \int_0^t \left(L(\tau) + \frac{\gamma l e^D}{c} U^2(\tau) \right) d\tau \right) \tag{143}$$

where $l > \frac{2\lambda_{\max}(PBB^T P)}{\lambda_{\min}(Q)}$, and L is a functional of $(Z(t), U(\theta))$, for all $t - D \leq \theta \leq t$, such that

$$L(t) \geq l\gamma \left(\frac{\lambda_{\min}(Q)}{4} |\xi(t)|^2 + \frac{1}{2} \|w(t)\|^2 \right) \tag{144}$$

for an arbitrary $\gamma > 0$.

Proof. Let

$$L(t) = -\frac{\gamma l e^D}{c+1} \alpha_1^2 (G^{-1}(\eta(D, t))) - \gamma \left(-\xi^T(t) Q \xi(t) + 2\xi^T(t) P B w(0, t) - l w^2(0, t) - l \int_0^D e^x w^2(x, t) dx \right), \tag{145}$$

where $l > \frac{2\lambda_{\max}(PBB^T P)}{\lambda_{\min}(Q)}$. It can be deduced that

$$\begin{aligned}
L(t) &\geq -\frac{\gamma l e^D}{c+1} \alpha_1^2 (G^{-1}(\eta(D, t))) - \gamma \left(-\lambda_{\min}(Q) \xi^T(t) \xi(t) + \frac{\lambda_{\min}(Q)}{2\lambda_{\max}(PBB^T P)} \xi^T(t) P B B^T P \xi(t) \right. \\
&\quad \left. + \frac{2\lambda_{\max}(PBB^T P)}{\lambda_{\min}(Q)} w^2(0, t) - l w^2(0, t) - l \int_0^D e^x w^2(x, t) dx \right) \\
&\geq -\frac{\gamma l e^D}{c+1} \alpha_1^2 (G^{-1}(\eta(D, t))) + \frac{\gamma \lambda_{\min}(Q)}{2} |\xi(t)|^2 + l\gamma \|w(t)\|^2.
\end{aligned} \tag{146}$$

From (87), (111), we know

$$\begin{aligned}
\alpha_1^2 (G^{-1}(\eta(D, t))) &= \left(-\sum_{i=1}^n \binom{n}{i-1} \eta_i(D, t) \right)^2 \\
&\leq (2^n - 1)^2 \left(e^D |h(t)| + \max \left\{ D, \frac{D^2}{2!}, \dots, \frac{D^n}{n!} \right\} \sqrt{D} \|u(t)\| \right)^2 \\
&\leq (2^n - 1)^2 (2e^{2D} |h(t)|^2 + 2e^{2D} D \|u(t)\|^2).
\end{aligned} \tag{147}$$

With the help of (115), (119), we arrive at

$$\begin{aligned} \alpha_1^2 (G^{-1}(\eta(D, t))) &\leq 2e^{2D}(2^n - 1)^2 (|h(t)|^2 + D\|u(t)\|^2) \\ &\leq 2e^{2D}(2^n - 1)^2 \left(\frac{4^n - 1}{3} + \frac{2nD(e^{2|A|D} - 1)}{|A|} \right) |\xi(t)|^2 \\ &\quad + 4De^{2D}(2^n - 1)^2 \left(1 + \frac{n|B|^2}{|A|} \left(\frac{e^{2|A|D} - 1}{2|A|} - D \right) \right) \|w(t)\|^2. \end{aligned} \tag{148}$$

Choosing

$$c^{**} = \max \left\{ \frac{8le^{3D}(2^n - 1)^2 \left(\frac{4^n - 1}{3} + \frac{2nD(e^{2|A|D} - 1)}{|A|} \right)}{\lambda_{\min} Q}, 8De^{3D}(2^n - 1)^2 \left(1 + \frac{n|B|^2}{|A|} \left(\frac{e^{2|A|D} - 1}{2|A|} - D \right) \right), c^* \right\}, \tag{149}$$

where c^* is given by (122), for all $c > c^{**}$, by (146), (148), it holds

$$L(t) \geq \frac{l\gamma\lambda_{\min}(Q)}{4} |\xi(t)|^2 + \frac{l\gamma}{2} \|w(t)\|^2. \tag{150}$$

Noting $U^*(t) = \frac{c}{c+1}\alpha_1(G^{-1}(\eta(D, t)))$, after some calculations, we have

$$\begin{aligned} L(t) &= -\frac{\gamma le^D}{c+1}\alpha_1^2(G^{-1}(\eta(D, t))) - \gamma \left(-\xi^T(t)Q\xi(t) + 2\xi^T(t)PBw(0, t) - lw^2(0, t) - l \int_0^D e^x w^2(x, t) dx \right) \\ &= -\frac{\gamma le^D}{c+1}\alpha_1^2(G^{-1}(\eta(D, t))) + \gamma le^D w^2(D, t) - \gamma \dot{V}(t) \\ &= -\frac{\gamma le^D}{c+1}\alpha_1^2(G^{-1}(\eta(D, t))) + \gamma le^D (U(t) - \alpha_1(G^{-1}(\eta(D, t))))^2 - \gamma \dot{V}(t) \\ &= -\frac{\gamma le^D(c+1)}{c^2} (U^*(t))^2 + \gamma le^D \left(U(t) - \frac{c+1}{c} U^*(t) \right)^2 - \gamma \dot{V}(t) \\ &= \frac{\gamma le^D}{c} (U^*(t))^2 + \gamma le^D \left((U(t) - U^*(t))^2 - \frac{2}{c} U(t)U^*(t) \right) - \gamma \dot{V}(t), \end{aligned} \tag{151}$$

and hence, it can be deduced that

$$\gamma V(t) + \int_0^t \left(L(\tau) + \frac{\gamma le^D}{c} U^2(\tau) \right) d\tau = \gamma V(0) + \gamma le^D \int_0^t \left(1 + \frac{1}{c} \right) (U(t) - U^*(t))^2 d\tau \tag{152}$$

so the minimum of (143) is reached with

$$U(t) = U^*(t) \tag{153}$$

such that

$$J = \gamma V(0). \tag{154}$$

The proof is completed. □

4 | EXAMPLE

Example 1. Consider a strict-feedforward nonlinear system given by Krstic⁶ as

$$\dot{Z}_1(t) = Z_2(t) + Z_3^2(t) \tag{155}$$

$$\dot{Z}_2(t) = Z_3(t) + Z_3(t)U(t - D) \tag{156}$$

$$\dot{Z}_3(t) = U(t - D), \tag{157}$$

where $Z_1, Z_2, Z_3 \in R$ are the states, U is a scalar control input, and $D \in R^+$ is an actuator delay. It is illustrated in the aforementioned work⁶ that the overall system (155)-(157) is not linearizable.

The nominal control design ($D = 0$) for system (155)-(157) is obtained by Krstic⁶ as

$$U(t) = -Z_1(t) - 3Z_2(t) - 3Z_3(t) - \frac{3}{8}Z_2^2(t) + \frac{3}{4}Z_3(t) \left(-Z_1(t) - 2Z_2(t) + \frac{1}{2}Z_3(t) + \frac{1}{2}Z_2(t)Z_3(t) + \frac{5}{8}Z_3^2(t) - \frac{1}{8}Z_3^3(t) - \frac{3}{8} \left(Z_2 - \frac{Z_3^2}{2} \right)^2 \right). \quad (158)$$

By Theorem 2, the predictor control for system (155)-(157) is designed as

$$U(t) = \frac{c}{c+1}U_1(t) = U^*(t), \quad (159)$$

where $c > 0$ is sufficiently large and

$$U_1(t) = -P_1(t) - 3P_2(t) - 3P_3(t) - \frac{3}{8}P_2^2(t) + \frac{3}{4}P_3(t) \left(-P_1(t) - 2P_2(t) + \frac{1}{2}P_3(t) + \frac{1}{2}P_2(t)P_3(t) + \frac{5}{8}P_3^2(t) - \frac{1}{8}P_3^3(t) - \frac{3}{8} \left(P_2 - \frac{P_3^2}{2} \right)^2 \right), \quad (160)$$

and $P_1(t) = p_1(D, t)$, $P_2(t) = p_2(D, t)$, and $P_3(t) = p_3(D, t)$ are provided for $x = D$ by

$$p_1(x, t) = Z_1(t) + \int_0^x (p_2(y, t) + p_3^2(y, t)) dy \quad (161)$$

$$p_2(x, t) = Z_2(t) + \int_0^x (p_3(y, t) + p_3^2(y, t)u(y, t)) dy \quad (162)$$

$$p_3(x, t) = Z_3(t) + \int_0^x u(y, t) dy. \quad (163)$$

Responses of the states of system (155)-(157) under the control law (159) are shown for $c = 100$ in Figure 1. One can observe that the closed-loop system is asymptotically stable. By Theorem 3, the control law (159) is inverse optimal.

Example 2. Consider a cart with an inverted pendulum system given by Wei²¹ as follows:

$$(m_1 + m_2)\ddot{q}_1 + m_2l \cos(q_2)\ddot{q}_2 = m_2l \sin(q_2)\dot{q}_2^2 + F \quad (164)$$

$$\cos(q_2)\ddot{q}_1 + l\ddot{q}_2 = g \sin(q_2), \quad (165)$$

where m_1 and q_1 are the mass and position of the cart; m_2 , l , and $q_2 \in (-\pi/2, \pi/2)$ are the mass, length of the link,

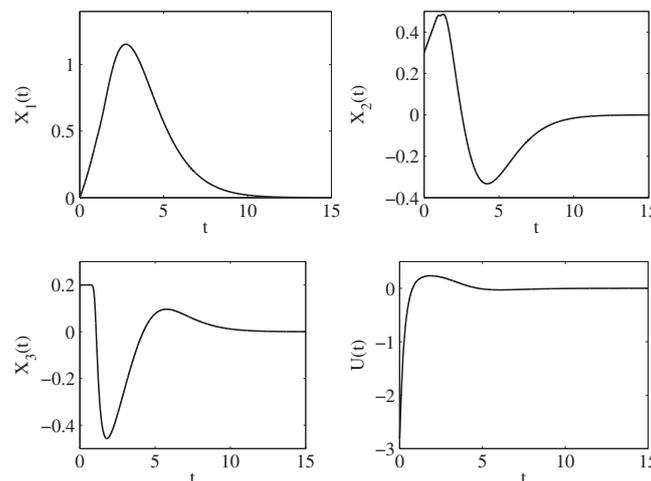


FIGURE 1 Responses of the states $X_1(t)$, $X_2(t)$, $X_3(t)$ of system (155)-(157) with the control law (159) for initial conditions as $X_1(0) = 0$, $X_2(0) = 0.3$, $X_3(0) = 0.2$ and $U(0) = 0$, for $\theta \in [0, 1]$

and angle of the pole, respectively, and $g = 9.8$ is the acceleration of gravity. Let $\dot{q}_2 = p_2$, $\dot{p}_2 = u$. Applying the feedback law (see the work of Wei²¹)

$$F = -ul (m_1 + m_2 \sin^2(q_2)) / \cos(q_2) + (m_1 + m_2)g \tan(q_2) - m_2 l \sin(q_2) \dot{q}_2^2 \quad (166)$$

and with the following global change of coordinates

$$x_1 = \lambda \left(q_1 + l \ln \left(\frac{1 + \tan(q_2/2)}{1 - \tan(q_2/2)} \right) \right) \quad (167)$$

$$x_2 = \dot{q}_1 + (l / \cos(q_2)) p_2, \quad (168)$$

we get

$$\dot{x}_1 = \lambda x_2 \quad (169)$$

$$\dot{x}_2 = \tan(q_2) \left(g + \frac{l}{\cos(q_2)} p_2^2 \right) \quad (170)$$

$$\dot{q}_2 = p_2 \quad (171)$$

$$\dot{p}_2 = u, \quad (172)$$

where $\lambda > 0$. To map the upper half-plane to R , we use another global change of coordinates and control as follows:

$$x_3 = \tan(q_2) \quad (173)$$

$$x_4 = (1 + \tan^2(q_2)) p_2 \quad (174)$$

$$v = (1 + x_3^2) u + \frac{2x_3 x_4^2}{(1 + x_3^2)} + \left(g x_3 + \frac{g}{2} x_4 \right) \sqrt{1 + x_3^2}. \quad (175)$$

Finally, the dynamics of the cart-pole system is transformed into the following (assuming $l = 1$):

$$\dot{x}_1 = \lambda x_2 \quad (176)$$

$$\dot{x}_2 = x_3 \left(g + \frac{x_4^2}{(1 + x_3^2)^{3/2}} \right) \quad (177)$$

$$\dot{x}_3 = x_4 \quad (178)$$

$$\dot{x}_4 = -(g x_3 + (g/2) x_4) \sqrt{1 + x_3^2} + v. \quad (179)$$

From the aforementioned work,²¹ the control law

$$v = v_1 + v_2 \quad (180)$$

$$v_1 = -2x_4 - x_3 - \left(1 / \sqrt{1 + x_3^2} \right) z_1 \quad (181)$$

$$z_1 = x_2 + \left(x_4 / \sqrt{1 + x_3^2} \right) + (g/2) x_3 \quad (182)$$

$$v_2 = \mu_2^{-1} \left(\frac{1}{2} x_3 \sqrt{1 + x_3^2} - x_4 \sqrt{1 + x_3^2} - \frac{1}{2} x_2 \right) - \mu_2 z_2 \quad (183)$$

$$z_2 = x_1 - N_2 \quad (184)$$

$$N_2 = -x_2 - \frac{g}{2} x_3 - \frac{1}{2g} x_4 - \frac{x_4}{\sqrt{1 + x_3^2}} - \frac{5}{4} \left(\frac{x_3 \sqrt{1 + x_3^2}}{2} + \frac{1}{2} \ln \left(x_3 + \sqrt{1 + x_3^2} \right) \right) \quad (185)$$

$$\mu_2 = \frac{1}{2g} + \frac{1}{\sqrt{1 + x_3^2}} \quad (186)$$

globally asymptotically stabilizes system (176)-(179).

We consider system (176)-(179) with input delay as follows:

$$\dot{x}_1 = \lambda x_2 \quad (187)$$

$$\dot{x}_2 = x_3 \left(g + \frac{x_4^2}{(1+x_3^2)^{3/2}} \right) \quad (188)$$

$$\dot{x}_3 = x_4 \quad (189)$$

$$\dot{x}_4 = -(gx_3 + (g/2)x_4) \sqrt{1+x_3^2} + U(t-D), \quad (190)$$

where $D \in R^+$ is an actuator delay.

By Theorem 2, the control law for system (187)-(190) is given by

$$U(t) = \frac{c}{c+1} U_1(t) = U^*(t), \quad (191)$$

where $c > 0$ is sufficiently large, and $U_1(t) = v(t)$ is given as (180)-(186) by replacing $x_i(t)$, $i = 1, 2, 3, 4$, with $P_i(t)$, $i = 1, 2, 3, 4$, and $P_1(t) = p_1(D, t)$, $P_2(t) = p_2(D, t)$, $P_3(t) = p_3(D, t)$, and $P_4(t) = p_4(D, t)$ are provided for $x = D$ by

$$p_1(x, t) = x_1(t) + \int_0^x \lambda p_2(y, t) dy \quad (192)$$

$$p_2(x, t) = x_2(t) + \int_0^x \left(p_3(y, t) \left(g + \frac{p_4^2(y, t)}{(1+p_3^2(y, t))^{3/2}} \right) \right) dy \quad (193)$$

$$p_3(x, t) = x_3(t) + \int_0^x p_4(y, t) dy \quad (194)$$

$$p_4(x, t) = x_4(t) + \int_0^x -(gp_3(y, t) + (g/2)p_4(y, t)) \sqrt{1+p_3^2(y, t)} + u(y, t) dy. \quad (195)$$

Figures 2 and 3 show the simulation results for the cart-pole system with the initial state $(q_1, p_1, q_2, p_2) = (5, 0, \pi/3, 0)$ (ie, $(x_1, x_2, x_3, x_4) = (2.5 + 0.5\ln(\frac{\sqrt{3}+1}{\sqrt{3}-1}), 0, \sqrt{3}, 0)$), and $c = 100$. In Figure 4, clearly, the control law (191) stabilizes the inverted pendulum in its upright position after a rather short time. The parameters are chosen as $m_1 = m_2 = l = 1$.

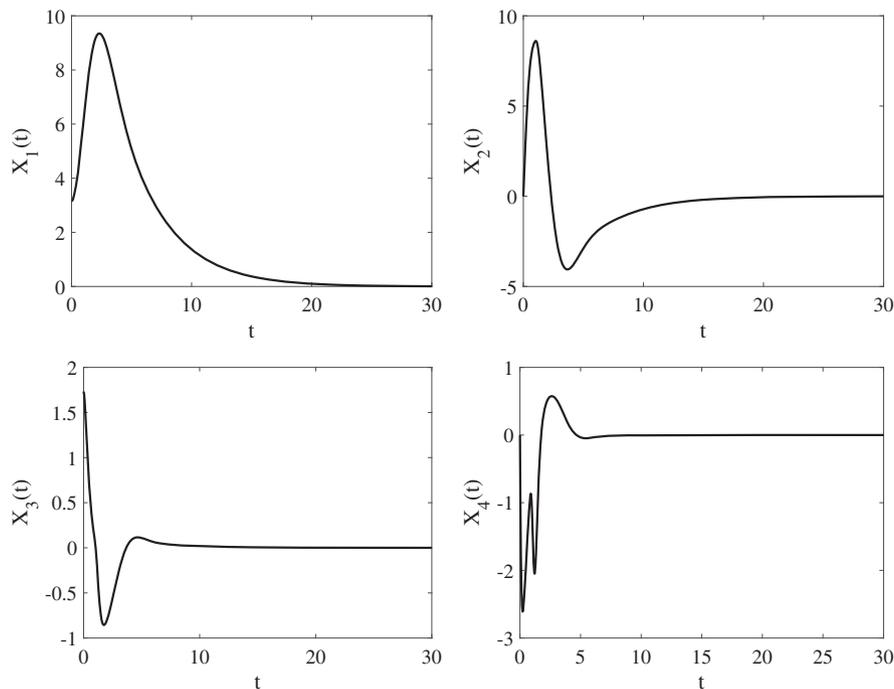


FIGURE 2 State trajectory of system (187)-(190)

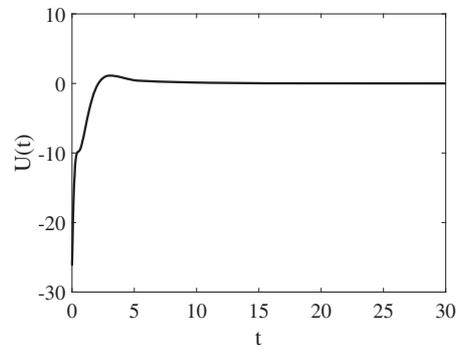


FIGURE 3 Control law (191)

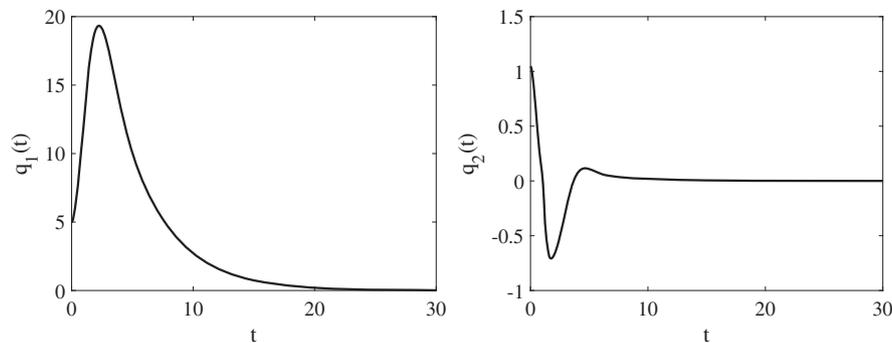


FIGURE 4 Position of the cart-pole system (164)-(165)

5 | CONCLUSIONS

Inverse optimal control for strict-feedforward systems with input delays is studied in this paper. A basic predictor control is designed for compensation for this class of nonlinear systems. Furthermore, it is shown that it is inverse optimal with respect to a meaningful differential game problem. For a class of linearizable strict-feedforward system, an explicit formula for compensation for input delay, which is also inverse optimal with respect to a meaningful differential game problem, is also obtained. A cart with an inverted pendulum system is given to illustrate the validity of the proposed method.

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REFERENCES

1. Mazenc F, Praly L. Adding integrations, saturated controls, and stabilization of feedforward systems. *IEEE Trans Autom Control*. 1996;41(11):1559-1578.
2. Sepulchre R, Jankovic M, Kokotovic PV. Integrator forwarding: a new recursive nonlinear robust design. *Automatica*. 1997;33(5):979-984.
3. Arcak M, Teel A, Kokotovic PV. Robust nonlinear control of feedforward systems with unmodeled dynamics. *Automatica*. 2001;37(2):265-272.
4. Xudong Y. Universal stabilization of feedforward nonlinear systems. *Automatica*. 2003;39(10):141-147.
5. Krstic M. Feedback linearizability and explicit integrator forwarding controllers for classes of feedforward systems. *IEEE Trans Autom Control*. 2004;49(10):1668-1682.
6. Krstic M. Input delay compensation for forward complete and strict-feedforward nonlinear systems. *IEEE Trans Autom Control*. 2010;55(2):287-303.
7. Krstic M. Lyapunov tools for predictor feedbacks for delay systems: inverse optimality and robustness to delay mismatch. *Automatica*. 2008;44(11):2930-2935.
8. Artstein Z. Linear systems with delayed controls: a reduction. *IEEE Trans Autom Control*. 1982;27(4):869-879.
9. Manitius AZ, Olbrot AW. Finite spectrum assignment problem for systems with delays. *IEEE Trans Autom Control*. 1979;24(4):541-553.

10. Mondie S, Michiels W. Finite spectrum assignment of unstable time-delay systems with a safe implementation. *IEEE Trans Autom Control*. 2003;48(12):2207-2212.
11. Bresch-Pietri D, Petit N. Robust compensation of a chattering time-varying input delay. Paper presented at: 53rd IEEE Conference on Decision and Control; 2014; Los Angeles, CA.
12. Mazenc F, Malisoff M, Niculescu SI. Stability and control design for time-varying systems with time-varying delays using a trajectory based approach. *SIAM J Control Optim*. 2017;55(1):533-556.
13. Bekiaris-Liberis N, Krstic M. Compensation of time-varying input and state delays for nonlinear systems. *J Dyn Syst Meas Control*. 2012;134(1):1-14.
14. Bekiaris-Liberis N, Krstic M. Robustness of nonlinear predictor feedback laws to time- and state-dependent delay perturbations. *Automatica*. 2013;49(6):1576-1590.
15. Cai X, Lin Y, Liu L. Universal stabilisation design for a class of non-linear systems with time-varying input delays. *IET Control Theory Appl*. 2015;9(10):1481-1490.
16. Bekiaris-Liberis N, Krstic M. Compensation of wave actuator dynamics for nonlinear systems. *IEEE Trans Autom Control*. 2014;59(6):1555-1570.
17. Cai X, Krstic M. Nonlinear control under wave actuator dynamics with time- and state-dependent moving boundary. *Int J Robust Nonlinear Control*. 2015;25(2):222-253.
18. Cai X, Krstic M. Nonlinear stabilization through wave PDE dynamics with a moving uncontrolled boundary. *Automatica*. 2016;68:27-38.
19. Karafyllis I, Krstic M. *Predictor Feedback for Delay Systems: Implementations and Approximations*. Cham, Switzerland: Springer; 2016.
20. Krstic M, Li Z. Inverse optimal design of input-to-state stabilizing nonlinear controllers. *IEEE Trans Autom Control*. 1998;43(3):336-350.
21. Wei X. The optimal stabilization of cart-pole system: A modified forwarding control method. Paper presented at: Proceedings of the IITA International Conference on Services Science, Management and Engineering; 2009; Zhangjiajie, China.

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